MATH 461: Fourier Series and Boundary Value Problems

Chapter IV: Vibrating Strings and Membranes

Greg Fasshauer

Department of Applied Mathematics Illinois Institute of Technology

Fall 2015



Outline

- Derivation of Vertically Vibrating Strings
- Boundary Conditions
- Example: Vibrating String with Fixed Ends
- Membranes (omitted now, done later in Chapter 7)



Outline

- Derivation of Vertically Vibrating Strings
- 2 Boundary Conditions
- 3 Example: Vibrating String with Fixed Ends
- 4 Membranes (omitted now, done later in Chapter 7)



Vibrating Strings

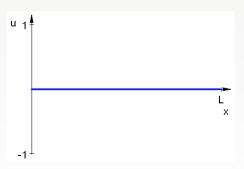
We will now derive a new mathematical model.



Vibrating Strings

We will now derive a new mathematical model.

Consider a stretched elastic string of length *L* with equilibrium position along the *x*-axis.





Vibrating Strings

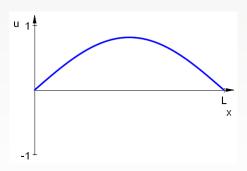
We will now derive a new mathematical model.

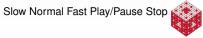
Consider a stretched elastic string of length *L* with equilibrium position along the *x*-axis.

Every point (x,0), $0 \le x \le L$, of the string has a displacement

$$y = u(x, t)$$

at any given time t > 0.







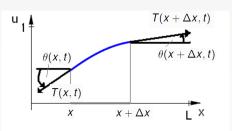
 We consider only small displacements (relative to the length of the string).



- We consider only small displacements (relative to the length of the string).
- This implies that we can neglect horizontal displacements.



- We consider only small displacements (relative to the length of the string).
- This implies that we can neglect horizontal displacements.
- We assume a perfectly flexible string, i.e., only tangential forces are acting on the string (see the figure).



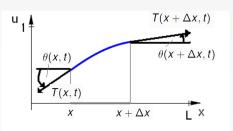




- We consider only small displacements (relative to the length of the string).
- This implies that we can neglect horizontal displacements.
- We assume a perfectly flexible string, i.e., only tangential forces are acting on the string (see the figure).

Herè we denote by

- T the (tangential) tension,
- θ the angle T forms with the horizontal (measured counter-clockwise).



For a small segment from x to $x + \Delta x$ we will use Newton's law

F = ma



For a small segment from x to $x + \Delta x$ we will use Newton's law

$$F = ma$$

coupled with a conservation law that balances the forces in a segment of the string as

```
{total force according to Newton}

=
{vertical force at left end of segment}

+
{vertical force at right end of segment}

+
{vertical component of body force (or possible external force)}
```



For a small segment from x to $x + \Delta x$ we will use Newton's law

$$F = ma$$

coupled with a conservation law that balances the forces in a segment of the string as

{total force according to Newton} =

{vertical force at left end of segment}

+

{vertical force at right end of segment}

+

{vertical component of body force (or possible external force)}

or

$$ma = V_L + V_R + V_{body}$$

to derive a PDE for the displacement u = u(x, t)



mass:

$$m(x) = \underbrace{\rho_0(x)}_{\text{density}} \Delta x$$





mass:

$$m(x) = \underbrace{\rho_0(x)}_{\text{density}} \Delta x$$

acceleration:

$$a(x,t) = \frac{\partial^2 u}{\partial t^2}(x,t)$$



mass:

$$m(x) = \underbrace{\rho_0(x)}_{\text{density}} \Delta x$$

acceleration:

$$a(x,t) = \frac{\partial^2 u}{\partial t^2}(x,t)$$

body force:

$$V_{body}(x,t) = \rho_0(x) \Delta x Q(x,t)$$

with Q(x, t) the vertical component of the body force per unit mass





mass:

$$m(x) = \underbrace{\rho_0(x)}_{\text{density}} \Delta x$$

acceleration:

$$a(x,t) = \frac{\partial^2 u}{\partial t^2}(x,t)$$

body force:

$$V_{body}(x,t) = \rho_0(x) \Delta x Q(x,t)$$

with Q(x, t) the vertical component of the body force per unit mass

A commonly used body force is $V_{body} = -mg$.





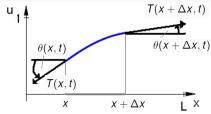
Since the displacement and motion are assumed to happen only in the vertical direction we require only the vertical component of the tensile force:



Since the displacement and motion are assumed to happen only in the vertical direction we require only the vertical component of the tensile force:

At the left end:

$$V_L(x,t) = -T(x,t)\sin\theta(x,t)$$







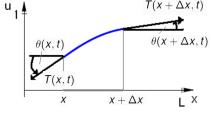
Since the displacement and motion are assumed to happen only in the vertical direction we require only the vertical component of the tensile force:

At the left end:

$$V_L(x,t) = -T(x,t)\sin\theta(x,t)$$

At the right end:

$$V_B(x, t) = T(x + \Delta x, t) \sin \theta(x + \Delta x, t)$$



$$\rho_0(x)\Delta x \frac{\partial^2 u}{\partial t^2}(x,t) = V_L(x,t) + V_R(x,t) + \rho_0(x)\Delta x Q(x,t)$$



$$\rho_0(x)\Delta x \frac{\partial^2 u}{\partial t^2}(x,t) = V_L(x,t) + V_R(x,t) + \rho_0(x)\Delta x Q(x,t)$$

$$= -T(x,t)\sin\theta(x,t) + T(x+\Delta x,t)\sin\theta(x+\Delta x,t)$$

$$+\rho_0(x)\Delta x Q(x,t)$$



$$\rho_0(x)\Delta x \frac{\partial^2 u}{\partial t^2}(x,t) = V_L(x,t) + V_R(x,t) + \rho_0(x)\Delta x Q(x,t)$$

$$= -T(x,t)\sin\theta(x,t) + T(x+\Delta x,t)\sin\theta(x+\Delta x,t)$$

$$+\rho_0(x)\Delta x Q(x,t)$$

If we divide by Δx we get

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \frac{T(x+\Delta x,t)\sin\theta(x+\Delta x,t) - T(x,t)\sin\theta(x,t)}{\Delta x} + \rho_0(x)Q(x,t)$$



$$\rho_0(x)\Delta x \frac{\partial^2 u}{\partial t^2}(x,t) = V_L(x,t) + V_R(x,t) + \rho_0(x)\Delta x Q(x,t)$$

$$= -T(x,t)\sin\theta(x,t) + T(x+\Delta x,t)\sin\theta(x+\Delta x,t)$$

$$+\rho_0(x)\Delta x Q(x,t)$$

If we divide by Δx and let Δx go to zero we get

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \underbrace{\frac{T(x+\Delta x,t)\sin\theta(x+\Delta x,t)-T(x,t)\sin\theta(x,t)}{\Delta x}}_{\qquad \qquad \qquad \qquad \rightarrow \frac{\partial}{\partial x}[T(x,t)\sin\theta(x,t)] \text{ as } \Delta x \rightarrow 0}_{\qquad \qquad +\rho_0(x)Q(x,t)}$$





$$\rho_0(x)\Delta x \frac{\partial^2 u}{\partial t^2}(x,t) = V_L(x,t) + V_R(x,t) + \rho_0(x)\Delta x Q(x,t)$$

$$= -T(x,t)\sin\theta(x,t) + T(x+\Delta x,t)\sin\theta(x+\Delta x,t)$$

$$+\rho_0(x)\Delta x Q(x,t)$$

If we divide by Δx and let Δx go to zero we get

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \underbrace{\frac{T(x+\Delta x,t)\sin\theta(x+\Delta x,t)-T(x,t)\sin\theta(x,t)}{\Delta x}}_{+\rho_0(x)Q(x,t)}$$

i.e.,

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \frac{\partial}{\partial x}\left[T(x,t)\sin\theta(x,t)\right] + \rho_0(x)Q(x,t).$$



Since the vertical displacement is assumed to be small, the angle $\theta(x, t)$ is also small (so that $\cos \theta(x, t) \approx 1$).



Since the vertical displacement is assumed to be small, the angle $\theta(x,t)$ is also small (so that $\cos\theta(x,t)\approx 1$). Therefore,

$$\sin \theta(x,t) \approx \frac{\sin \theta(x,t)}{\cos \theta(x,t)} = \tan \theta(x,t)$$



Since the vertical displacement is assumed to be small, the angle $\theta(x,t)$ is also small (so that $\cos\theta(x,t)\approx 1$).

$$\sin \theta(x,t) \approx \frac{\sin \theta(x,t)}{\cos \theta(x,t)} = \tan \theta(x,t)$$

Here it is important to note that $\tan \theta(x, t)$ corresponds to the "slope" of the string, i.e.,

$$\tan \theta(x,t) = \frac{\partial u}{\partial x}(x,t).$$



Therefore.

Since the vertical displacement is assumed to be small, the angle $\theta(x,t)$ is also small (so that $\cos\theta(x,t)\approx 1$).

Therefore,

$$\sin \theta(x,t) \approx \frac{\sin \theta(x,t)}{\cos \theta(x,t)} = \tan \theta(x,t)$$

Here it is important to note that $\tan \theta(x, t)$ corresponds to the "slope" of the string, i.e.,

$$\tan\theta(x,t)=\frac{\partial u}{\partial x}(x,t).$$

Thus

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \frac{\partial}{\partial x}\left[T(x,t)\sin\theta(x,t)\right] + \rho_0(x)Q(x,t)$$



Since the vertical displacement is assumed to be small, the angle $\theta(x,t)$ is also small (so that $\cos\theta(x,t)\approx 1$).

Therefore,

$$\sin \theta(x,t) \approx \frac{\sin \theta(x,t)}{\cos \theta(x,t)} = \tan \theta(x,t)$$

Here it is important to note that $\tan \theta(x, t)$ corresponds to the "slope" of the string, i.e.,

$$\tan\theta(x,t)=\frac{\partial u}{\partial x}(x,t).$$

Thus

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \frac{\partial}{\partial x}\left[T(x,t)\sin\theta(x,t)\right] + \rho_0(x)Q(x,t)$$

turns into the PDE for the vibrating string

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = \frac{\partial}{\partial x}\left[T(x,t)\frac{\partial u}{\partial x}(x,t)\right] + \rho_0(x)Q(x,t).$$





 Small displacements and perfectly elastic strings imply an approximately constant tension, i.e.,

$$T(x,t) \approx T_0 = \text{const.}$$



 Small displacements and perfectly elastic strings imply an approximately constant tension, i.e.,

$$T(x,t) \approx T_0 = \text{const.}$$

So

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = T_0\frac{\partial^2 u}{\partial x^2}(x,t) + \rho_0(x)Q(x,t)$$



 Small displacements and perfectly elastic strings imply an approximately constant tension, i.e.,

$$T(x,t) \approx T_0 = \text{const.}$$

So

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = T_0\frac{\partial^2 u}{\partial x^2}(x,t) + \rho_0(x)Q(x,t)$$

 Often the external force term can be neglected because the weight of the string is small compared to the tension so that there is no "sag" in the string.



In order to get the commonly used version of the 1D wave equation we make two further assumptions:

 Small displacements and perfectly elastic strings imply an approximately constant tension, i.e.,

$$T(x,t) \approx T_0 = \text{const.}$$

So

$$\rho_0(x)\frac{\partial^2 u}{\partial t^2}(x,t) = T_0\frac{\partial^2 u}{\partial x^2}(x,t) + \rho_0(x)Q(x,t)$$

 Often the external force term can be neglected because the weight of the string is small compared to the tension so that there is no "sag" in the string. Then we have

$$\frac{\partial^2 u}{\partial t^2}(x,t) = c^2 \frac{\partial^2 u}{\partial x^2}(x,t) \quad \text{with } c^2 = \frac{T_0}{\rho_0(x)},$$

the 1D wave equation.



Since the 1D wave equation contains

- a second-order spatial derivative term and
- a second-order time derivative term



Since the 1D wave equation contains

- a second-order spatial derivative term and
- a second-order time derivative term

we need to specify

 two spatial conditions (as usual, we do this in the form of boundary conditions – see next section), and



Since the 1D wave equation contains

- a second-order spatial derivative term and
- a second-order time derivative term

we need to specify

- two spatial conditions (as usual, we do this in the form of boundary conditions – see next section), and
- two temporal conditions. These will be given as
 - initial position: u(x,0) = f(x) and
 - initial velocity: $\frac{\partial u}{\partial t}(x,0) = g(x)$.





Outline

- Derivation of Vertically Vibrating Strings
- Boundary Conditions
- 3 Example: Vibrating String with Fixed Ends
- 4 Membranes (omitted now, done later in Chapter 7)





Fixed Ends

The simplest form of boundary conditions is

$$u(0,t) = 0$$

$$\begin{array}{rcl} u(0,t) & = & 0 \\ u(L,t) & = & 0 \end{array}$$



Fixed Ends

The simplest form of boundary conditions is

$$u(0,t) = 0$$

$$u(L,t) = 0$$

We could also have ends that are affixed to a moving support. Then they would be of the form

$$u(0,t) = f_1(t)$$

$$u(L,t) = f_2(t)$$

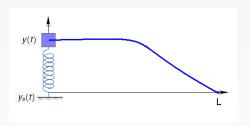




This will occur if a string is, e.g., attached to a spring-mass system

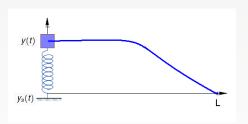


This will occur if a string is, e.g., attached to a spring-mass system





This will occur if a string is, e.g., attached to a spring-mass system



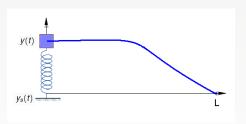
Thus

$$u(0,t)=y(t),$$

where y(t) is unknown. In fact, y is determined by an ODE for a spring-mass system with a possibly moving support $y_s(t)$.



This will occur if a string is, e.g., attached to a spring-mass system



Thus

$$u(0, t) = y(t),$$

where y(t) is unknown. In fact, y is determined by an ODE for a spring-mass system with a possibly moving support $y_s(t)$. Note that – to keep things manageable – we assume that the spring-mass system moves only vertically.



$$m \frac{\mathrm{d}^2 y}{\mathrm{d}t^2}(t) = -k \left[y(t) - y_s(t) - \ell \right] + \text{other forces},$$

where

- k is the spring constant,
- $y_s(t)$ denotes the moving support of the spring, possibly driven by some external force,
- ℓ is the length of the unstretched spring.





$$m rac{\mathrm{d}^2 y}{\mathrm{d}t^2}(t) = -k \left[y(t) - y_s(t) - \ell
ight] + ext{other forces},$$

where

- *k* is the spring constant,
- $y_s(t)$ denotes the moving support of the spring, possibly driven by some external force,
- ullet is the length of the unstretched spring.

The "other forces" should include the vertical component of the tensile force of the string:

$$T(0,t)\sin\theta(0,t)$$



$$m rac{\mathrm{d}^2 y}{\mathrm{d}t^2}(t) = -k \left[y(t) - y_s(t) - \ell
ight] + ext{other forces},$$

where

- k is the spring constant,
- $y_s(t)$ denotes the moving support of the spring, possibly driven by some external force,
- ullet is the length of the unstretched spring.

The "other forces" should include the vertical component of the tensile force of the string:

$$T(0,t)\sin\theta(0,t) \stackrel{\text{small }\theta}{pprox} T_0\tan\theta(0,t)$$



$$m \frac{\mathrm{d}^2 y}{\mathrm{d}t^2}(t) = -k \left[y(t) - y_{\mathrm{s}}(t) - \ell \right] + \mathrm{other\ forces},$$

where

- *k* is the spring constant,
- $y_s(t)$ denotes the moving support of the spring, possibly driven by some external force,
- ullet is the length of the unstretched spring.

The "other forces" should include the vertical component of the tensile force of the string:

$$T(0,t)\sin\theta(0,t) \stackrel{\text{small } \theta}{\approx} T_0\tan\theta(0,t) = T_0\frac{\partial u}{\partial x}(0,t).$$



$$m \frac{\mathrm{d}^2 y}{\mathrm{d}t^2}(t) = -k \left[y(t) - y_s(t) - \ell \right] + \mathrm{other\ forces},$$

where

- k is the spring constant,
- $y_s(t)$ denotes the moving support of the spring, possibly driven by some external force,
- ℓ is the length of the unstretched spring.

The "other forces" should include the vertical component of the tensile force of the string:

$$T(0,t)\sin\theta(0,t) \stackrel{\text{small } \theta}{\approx} T_0\tan\theta(0,t) = T_0\frac{\partial u}{\partial x}(0,t).$$

Thus, elastic BCs are of the form

$$m\frac{\mathsf{d}^2 y}{\mathsf{d}t^2}(t) = -k\left[y(t) - y_{\mathsf{s}}(t) - \ell\right] + T_0\frac{\partial u}{\partial x}(0,t) + g(t).$$



In the special case

- g(t) = 0 (i.e., no additional external forces)
- with a spring-mass system with small mass, i.e., $m \approx 0$,
- and taking y(t) = u(0, t)

we get the BC

$$k[u(0,t)-y_s(t)-\ell] = T_0 \frac{\partial u}{\partial x}(0,t)$$



In the special case

- g(t) = 0 (i.e., no additional external forces)
- with a spring-mass system with small mass, i.e., $m \approx 0$,
- and taking y(t) = u(0, t)

we get the BC

$$k[u(0,t) - y_s(t) - \ell] = T_0 \frac{\partial u}{\partial x}(0,t)$$

$$\iff k[u(0,t) - y_E(t)] = T_0 \frac{\partial u}{\partial x}(0,t),$$

where $y_E(t) = y_s(t) + \ell$ denotes the equilibrium position of the spring-mass system.





If in addition $y_E(t) = 0$, i.e., the equilibrium position of the spring-mass system coincides with the equilibrium position of the string and occurs at the origin, then

$$k\left[u(0,t)-y_{E}(t)\right]=T_{0}\frac{\partial u}{\partial x}(0,t)$$



If in addition $y_E(t) = 0$, i.e., the equilibrium position of the spring-mass system coincides with the equilibrium position of the string and occurs at the origin, then

$$k\left[u(0,t)-y_{E}(t)\right]=T_{0}\frac{\partial u}{\partial x}(0,t)$$

becomes

$$T_0 \frac{\partial u}{\partial x}(0,t) = ku(0,t).$$





If in addition $y_E(t) = 0$, i.e., the equilibrium position of the spring-mass system coincides with the equilibrium position of the string and occurs at the origin, then

$$k\left[u(0,t)-y_{E}(t)\right]=T_{0}\frac{\partial u}{\partial x}(0,t)$$

becomes

$$T_0\frac{\partial u}{\partial x}(0,t)=ku(0,t).$$

Remark

Note that this BC is analogous to the one we obtained via Newton's law of cooling for the 1D heat equation.





Note that the tensile force and spring constant are usually positive, i.e., $T_0 > 0$, k > 0. Then we see from

$$T_0 \frac{\partial u}{\partial x}(0,t) = ku(0,t)$$
 that $u(0,t) > 0 \Longleftrightarrow \frac{\partial u}{\partial x}(0,t) > 0.$

Note that the tensile force and spring constant are usually positive, i.e., $T_0 > 0$, k > 0. Then we see from

$$T_0 \frac{\partial u}{\partial x}(0,t) = ku(0,t)$$
 that $u(0,t) > 0 \Longleftrightarrow \frac{\partial u}{\partial x}(0,t) > 0.$

However, at the right end, x = L, we will have

$$u(L,t) > 0 \Longleftrightarrow \frac{\partial u}{\partial x}(L,t) < 0,$$

i.e., upward motion pulls the string "inside".



Note that the tensile force and spring constant are usually positive, i.e., $T_0 > 0$, k > 0. Then we see from

$$T_0 \frac{\partial u}{\partial x}(0,t) = ku(0,t)$$
 that $u(0,t) > 0 \Longleftrightarrow \frac{\partial u}{\partial x}(0,t) > 0.$

However, at the right end, x = L, we will have

$$u(L,t) > 0 \Longleftrightarrow \frac{\partial u}{\partial x}(L,t) < 0,$$

i.e., upward motion pulls the string "inside". Therefore, the corresponding BC at the right end has a different sign and looks like

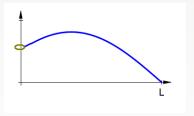
$$T_0 \frac{\partial u}{\partial x}(L,t) = -ku(L,t).$$



This will happen when the string is attached to a ring that slides frictionless along a vertical support.



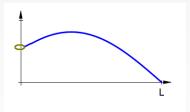
This will happen when the string is attached to a ring that slides frictionless along a vertical support.







This will happen when the string is attached to a ring that slides frictionless along a vertical support.



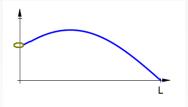
Physically, this corresponds to the limiting case of the spring-mass system for $k \to 0$, i.e.,

$$T_0\frac{\partial u}{\partial x}(0,t)=0.$$





This will happen when the string is attached to a ring that slides frictionless along a vertical support.



Physically, this corresponds to the limiting case of the spring-mass system for $k \to 0$, i.e.,

$$T_0\frac{\partial u}{\partial x}(0,t)=0.$$

Remark

Note the analogy to the insulated end condition for the heat equation.

Outline

- Derivation of Vertically Vibrating Strings
- 2 Boundary Conditions
- Example: Vibrating String with Fixed Ends
- 4 Membranes (omitted now, done later in Chapter 7)





We solve the PDE

$$\frac{\partial^2}{\partial t^2} u(x,t) = c^2 \frac{\partial^2}{\partial x^2} u(x,t), \quad \text{for } 0 < x < L, \ t > 0,$$
 (1)

with boundary conditions

$$u(0,t) = u(L,t) = 0$$
 for $t > 0$ (2)

and initial conditions

$$u(x,0) = f(x)$$
 for $0 < x < L$ (initial position) (3)

$$\frac{\partial u}{\partial t}(x,0) = g(x)$$
 for $0 < x < L$ (initial velocity) (4)





We solve the PDE

$$\frac{\partial^2}{\partial t^2} u(x,t) = c^2 \frac{\partial^2}{\partial x^2} u(x,t), \quad \text{for } 0 < x < L, \ t > 0,$$

with boundary conditions

$$u(0,t) = u(L,t) = 0$$
 for $t > 0$ (2)

and initial conditions

$$u(x,0) = f(x)$$
 for $0 < x < L$ (initial position) (3)

$$\frac{\partial u}{\partial t}(x,0) = g(x)$$
 for $0 < x < L$ (initial velocity) (4)

From our earlier derivations the constant $c^2 = \frac{T_0}{\rho_0}$ is given as the ratio of tension to density.

Since the PDE and its BCs are linear and homogeneous we attempt to solve the problem using separation of variables.



Since the PDE and its BCs are linear and homogeneous we attempt to solve the problem using separation of variables.

The usual *Ansatz* $u(x, t) = \varphi(x)T(t)$ gives us the partial derivatives

$$\frac{\partial^2}{\partial t^2} u(x,t) = \varphi(x) T''(t)$$
$$\frac{\partial^2}{\partial x^2} u(x,t) = \varphi''(x) T(t)$$



Since the PDE and its BCs are linear and homogeneous we attempt to solve the problem using separation of variables.

The usual *Ansatz* $u(x, t) = \varphi(x)T(t)$ gives us the partial derivatives

$$\frac{\partial^2}{\partial t^2} u(x,t) = \varphi(x) T''(t)$$
$$\frac{\partial^2}{\partial x^2} u(x,t) = \varphi''(x) T(t)$$

so that we have

$$\varphi(x)T''(t) = c^2 \varphi''(x)T(t)$$



Since the PDE and its BCs are linear and homogeneous we attempt to solve the problem using separation of variables.

The usual *Ansatz* $u(x, t) = \varphi(x)T(t)$ gives us the partial derivatives

$$\frac{\partial^2}{\partial t^2} u(x,t) = \varphi(x) T''(t)$$
$$\frac{\partial^2}{\partial x^2} u(x,t) = \varphi''(x) T(t)$$

so that we have

$$\varphi(x)T''(t) = c^2\varphi''(x)T(t)$$

or

$$\frac{1}{c^2}\frac{T''(t)}{T(t)} = \frac{\varphi''(x)}{\varphi(x)} = -\lambda.$$



The resulting two ODEs are

$$T''(t) = -\lambda c^2 T(t) \tag{5}$$

and

$$\varphi''(\mathbf{x}) = -\lambda \varphi(\mathbf{x}) \tag{6}$$

with BCs



The resulting two ODEs are

$$T''(t) = -\lambda c^2 T(t) \tag{5}$$

and

$$\varphi''(\mathbf{x}) = -\lambda \varphi(\mathbf{x}) \tag{6}$$

with BCs

$$\varphi(0) = \varphi(L) = 0. \tag{7}$$



The resulting two ODEs are

$$T''(t) = -\lambda c^2 T(t) \tag{5}$$

and

$$\varphi''(\mathbf{x}) = -\lambda \varphi(\mathbf{x}) \tag{6}$$

with BCs

$$\varphi(0) = \varphi(L) = 0. \tag{7}$$

Remark

We chose $-\lambda$ for the separation constant above so that (6)-(7) is one of our standard boundary-value problems with well-known eigenvalues and eigenfunctions

The resulting two ODEs are

$$T''(t) = -\lambda c^2 T(t) \tag{5}$$

and

$$\varphi''(\mathbf{x}) = -\lambda \varphi(\mathbf{x}) \tag{6}$$

with BCs

$$\varphi(0) = \varphi(L) = 0. \tag{7}$$

Remark

We chose $-\lambda$ for the separation constant above so that (6)-(7) is one of our standard boundary-value problems with well-known eigenvalues and eigenfunctions

$$\lambda_n = \left(\frac{n\pi}{L}\right)^2, \qquad \varphi_n(x) = \sin\frac{n\pi x}{L}, \quad n = 1, 2, 3, \dots$$

Remark

Moreover, the ODE (5) for the time-dependent component T has the physically meaningful, oscillating solution for positive λ , i.e.,

$$T(t) = c_1 \cos c \sqrt{\lambda} t + c_2 \sin c \sqrt{\lambda} t.$$



Remark

Moreover, the ODE (5) for the time-dependent component T has the physically meaningful, oscillating solution for positive λ , i.e.,

$$T(t) = c_1 \cos c \sqrt{\lambda} t + c_2 \sin c \sqrt{\lambda} t.$$

For this example the other two types of solution

•
$$T(t) = c_1 t + c_2$$
 for $\lambda = 0$

•
$$T(t) = c_1 e^{c\sqrt{-\lambda}t} + c_2 e^{-c\sqrt{-\lambda}t}$$
 for $\lambda < 0$

are not relevant.



$$u(x,t) = \sum_{n=1}^{\infty} \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$



$$u(x,t) = \sum_{n=1}^{\infty} \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

To determine the expansion coefficients A_n and B_n we use the initial conditions (3) and (4).



$$u(x,t) = \sum_{n=1}^{\infty} \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

To determine the expansion coefficients A_n and B_n we use the initial conditions (3) and (4).

Since $\cos 0 = 1$ and $\sin 0 = 0$ we have

$$u(x,0) = \sum_{n=1}^{\infty} A_n \sin \frac{n\pi x}{L} \stackrel{!}{=} f(x)$$





$$u(x,t) = \sum_{n=1}^{\infty} \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

To determine the expansion coefficients A_n and B_n we use the initial conditions (3) and (4).

Since $\cos 0 = 1$ and $\sin 0 = 0$ we have

$$u(x,0) = \sum_{n=1}^{\infty} A_n \sin \frac{n\pi x}{L} \stackrel{!}{=} f(x)$$

so that

$$A_n = \frac{2}{L} \int_0^L f(x) \sin \frac{n\pi x}{L} dx.$$





- u is continuous and
- $\frac{\partial u}{\partial t}$ is piecewise smooth.



- u is continuous and
- $\frac{\partial u}{\partial t}$ is piecewise smooth.

Then we can apply term-by-term differentiation to get

$$\frac{\partial u}{\partial t}(x,t) = \sum_{n=1}^{\infty} \left[-A_n \frac{cn\pi}{L} \sin \frac{cn\pi t}{L} + B_n \frac{cn\pi}{L} \cos \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$



- u is continuous and
- $\frac{\partial u}{\partial t}$ is piecewise smooth.

Then we can apply term-by-term differentiation to get

$$\frac{\partial u}{\partial t}(x,t) = \sum_{n=1}^{\infty} \left[-A_n \frac{cn\pi}{L} \sin \frac{cn\pi t}{L} + B_n \frac{cn\pi}{L} \cos \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

and

$$\frac{\partial u}{\partial t}(x,0) = \sum_{n=1}^{\infty} B_n \frac{cn\pi}{L} \sin \frac{n\pi x}{L} \stackrel{!}{=} g(x)$$



- u is continuous and
- $\frac{\partial u}{\partial t}$ is piecewise smooth.

Then we can apply term-by-term differentiation to get

$$\frac{\partial u}{\partial t}(x,t) = \sum_{n=1}^{\infty} \left[-A_n \frac{cn\pi}{L} \sin \frac{cn\pi t}{L} + B_n \frac{cn\pi}{L} \cos \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

and

$$\frac{\partial u}{\partial t}(x,0) = \sum_{n=1}^{\infty} B_n \frac{cn\pi}{L} \sin \frac{n\pi x}{L} \stackrel{!}{=} g(x)$$

so that

$$B_n = \frac{2}{cn\pi} \int_0^L g(x) \sin \frac{n\pi x}{L} dx.$$



- u is continuous and
- $\frac{\partial u}{\partial t}$ is piecewise smooth.

Then we can apply term-by-term differentiation to get

$$\frac{\partial u}{\partial t}(x,t) = \sum_{n=1}^{\infty} \left[-A_n \frac{cn\pi}{L} \sin \frac{cn\pi t}{L} + B_n \frac{cn\pi}{L} \cos \frac{cn\pi t}{L} \right] \sin \frac{n\pi x}{L}$$

and

$$\frac{\partial u}{\partial t}(x,0) = \sum_{n=1}^{\infty} B_n \frac{cn\pi}{L} \sin \frac{n\pi x}{L} \stackrel{!}{=} g(x)$$

so that

$$B_n = \frac{2}{cn\pi} \int_0^L g(x) \sin \frac{n\pi x}{L} dx.$$

The solution for this problem is illustrated in the Mathematica notebook

Normal Modes and Overtones: Applications to Music

For each *n*, the *n*-th term of the Fourier series solution

$$u_n(x,t) = \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L}\right] \sin \frac{n\pi x}{L}$$

is called the *n*-th normal mode of the solution.



Normal Modes and Overtones: Applications to Music

For each *n*, the *n*-th term of the Fourier series solution

$$u_n(x,t) = \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L}\right] \sin \frac{n\pi x}{L}$$

is called the *n*-th normal mode of the solution.

The term u_n describes a harmonic motion with frequency

$$f_n = \frac{cn\pi}{L}/2\pi = \frac{cn}{2L}$$

or with circular frequency $\omega = \frac{cn\pi}{L}$.



Normal Modes and Overtones: Applications to Music

For each *n*, the *n*-th term of the Fourier series solution

$$u_n(x,t) = \left[A_n \cos \frac{cn\pi t}{L} + B_n \sin \frac{cn\pi t}{L}\right] \sin \frac{n\pi x}{L}$$

is called the *n*-th normal mode of the solution.

The term u_n describes a harmonic motion with frequency

$$f_n = \frac{cn\pi}{L}/2\pi = \frac{cn}{2L}$$

or with circular frequency $\omega = \frac{cn\pi}{L}$.

The frequencies f_n are called the natural frequencies of the solution u

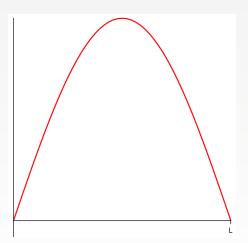


Figure: Fundamental mode, n = 1.



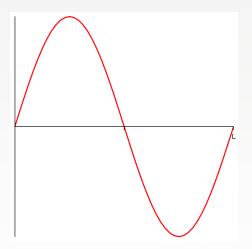


Figure: Second mode, or first overtone, n = 2.



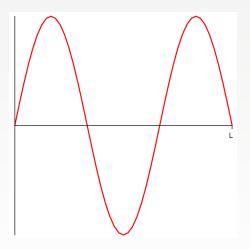


Figure: Third mode, or second overtone, n = 3.



$$\sin\frac{n\pi x}{L}=0,$$



$$\sin \frac{n\pi x}{I} = 0$$
, i.e., $\frac{n\pi x}{I} = k\pi$, $k = 1, 2, 3, ...$

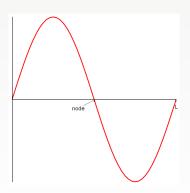


$$\sin \frac{n\pi x}{L} = 0$$
, i.e., $\frac{n\pi x}{L} = k\pi$, $k = 1, 2, 3, ...$

The points

$$x_k = k \frac{L}{n}, \quad k = 1, 2, \dots, n$$

are called nodes.



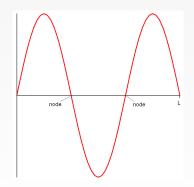


$$\sin \frac{n\pi x}{L} = 0$$
, i.e., $\frac{n\pi x}{L} = k\pi$, $k = 1, 2, 3, ...$

The points

$$x_k = k \frac{L}{n}, \quad k = 1, 2, \dots, n$$

are called nodes.



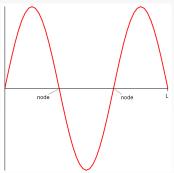


$$\sin \frac{n\pi x}{L} = 0$$
, i.e., $\frac{n\pi x}{L} = k\pi$, $k = 1, 2, 3, ...$

The points

$$x_k = k \frac{L}{n}, \quad k = 1, 2, \dots, n$$

are called nodes.



By placing their finger at a node point, players of string instruments such as guitars, violins, etc., can produce so-called flageolet tones.

MATH 461 - Chapter 4



• decreasing the length of the string, L, or



- decreasing the length of the string, L, or
- increasing *c*.



- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either



- decreasing the length of the string, L, or
- increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or



- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or
 - decrease the density of the string.



- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or
 - decrease the density of the string.

Remark

Overtones are illustrated acoustically in the MATLAB script overtones.m.

- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or
 - decrease the density of the string.

Remark

Overtones are illustrated acoustically in the MATLAB script overtones.m.

 We can hear there that the first overtone (i.e., with double the frequency) is an octave higher than the fundamental mode.

- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or
 - decrease the density of the string.

Remark

Overtones are illustrated acoustically in the MATLAB script overtones.m.

- We can hear there that the first overtone (i.e., with double the frequency) is an octave higher than the fundamental mode.
- Similarly, the second overtone is a fifth higher than the first overtone.

- decreasing the length of the string, L, or
- ullet increasing c. Since $c=\sqrt{rac{T_0}{
 ho_0}}$ this means that one can either
 - increase the tension or
 - decrease the density of the string.

Remark

Overtones are illustrated acoustically in the MATLAB script overtones.m.

- We can hear there that the first overtone (i.e., with double the frequency) is an octave higher than the fundamental mode.
- Similarly, the second overtone is a fifth higher than the first overtone,
- and the third overtone is a fourth higher than the second overtone.

Traveling Waves (Exercise 4.4.7)

Let's again consider the 1D wave equation

$$\frac{\partial^2}{\partial t^2} u(x,t) = c^2 \frac{\partial^2}{\partial x^2} u(x,t)$$

$$u(0,t) = u(L,t) = 0$$

$$u(x,0) = f(x) \text{ and } \frac{\partial u}{\partial t}(x,0) = g(x) = 0$$



Traveling Waves (Exercise 4.4.7)

Let's again consider the 1D wave equation

$$\frac{\partial^2}{\partial t^2} u(x,t) = c^2 \frac{\partial^2}{\partial x^2} u(x,t)$$

$$u(0,t) = u(L,t) = 0$$

$$u(x,0) = f(x) \text{ and } \frac{\partial u}{\partial t}(x,0) = g(x) = 0$$

From the general solution derived above we know that

$$B_n = \frac{2}{cn\pi} \int_0^L g(x) \sin \frac{n\pi x}{L} dx = 0.$$



Traveling Waves (Exercise 4.4.7)

Let's again consider the 1D wave equation

$$\frac{\partial^2}{\partial t^2} u(x,t) = c^2 \frac{\partial^2}{\partial x^2} u(x,t)$$

$$u(0,t) = u(L,t) = 0$$

$$u(x,0) = f(x) \text{ and } \frac{\partial u}{\partial t}(x,0) = g(x) = 0$$

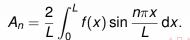
From the general solution derived above we know that

$$B_n = \frac{2}{cn\pi} \int_0^L g(x) \sin \frac{n\pi x}{L} dx = 0.$$

Therefore

$$u(x,t) = \sum_{n=1}^{\infty} A_n \cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L}$$

with





$$\sin \alpha \cos \beta = \frac{1}{2} \left[\sin(\alpha + \beta) + \sin(\alpha - \beta) \right]$$

with
$$\alpha = \frac{n\pi x}{L}$$
 and $\beta = \frac{cn\pi t}{L}$ gives us

$$\cos\frac{cn\pi t}{L}\sin\frac{n\pi x}{L} = \frac{1}{2}\left[\sin\left(\frac{n\pi x}{L} + \frac{cn\pi t}{L}\right) + \sin\left(\frac{n\pi x}{L} - \frac{cn\pi t}{L}\right)\right]$$



$$\sin \alpha \cos \beta = \frac{1}{2} \left[\sin(\alpha + \beta) + \sin(\alpha - \beta) \right]$$

with
$$\alpha = \frac{n\pi x}{L}$$
 and $\beta = \frac{cn\pi t}{L}$ gives us

$$\cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L} = \frac{1}{2} \left[\sin \left(\frac{n\pi x}{L} + \frac{cn\pi t}{L} \right) + \sin \left(\frac{n\pi x}{L} - \frac{cn\pi t}{L} \right) \right]$$
$$= \frac{1}{2} \left[\sin \frac{n\pi}{L} (x + ct) + \sin \frac{n\pi}{L} (x - ct) \right]$$



$$\sin \alpha \cos \beta = \frac{1}{2} \left[\sin(\alpha + \beta) + \sin(\alpha - \beta) \right]$$

with $\alpha = \frac{n\pi x}{L}$ and $\beta = \frac{cn\pi t}{L}$ gives us

$$\cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L} = \frac{1}{2} \left[\sin \left(\frac{n\pi x}{L} + \frac{cn\pi t}{L} \right) + \sin \left(\frac{n\pi x}{L} - \frac{cn\pi t}{L} \right) \right]$$
$$= \frac{1}{2} \left[\sin \frac{n\pi}{L} (x + ct) + \sin \frac{n\pi}{L} (x - ct) \right]$$

So the solution

$$u(x,t) = \sum_{n=1}^{\infty} A_n \cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L}$$



$$\sin \alpha \cos \beta = \frac{1}{2} \left[\sin(\alpha + \beta) + \sin(\alpha - \beta) \right]$$

with $\alpha = \frac{n\pi x}{L}$ and $\beta = \frac{cn\pi t}{L}$ gives us

$$\cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L} = \frac{1}{2} \left[\sin \left(\frac{n\pi x}{L} + \frac{cn\pi t}{L} \right) + \sin \left(\frac{n\pi x}{L} - \frac{cn\pi t}{L} \right) \right]$$
$$= \frac{1}{2} \left[\sin \frac{n\pi}{L} (x + ct) + \sin \frac{n\pi}{L} (x - ct) \right]$$

So the solution

$$u(x,t) = \sum_{n=1}^{\infty} A_n \cos \frac{cn\pi t}{L} \sin \frac{n\pi x}{L}$$

becomes

$$u(x,t) = \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x+ct) + \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x-ct)$$



Remark

Note that the two parts of

$$u(x,t) = \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x+ct) + \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x-ct)$$

are Fourier sine series of f evaluated at x + ct and x - ct, respectively.



Remark

Note that the two parts of

$$u(x,t) = \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x+ct) + \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x-ct)$$

are Fourier sine series of f evaluated at x + ct and x - ct, respectively.

Therefore

$$u(x,t)=\frac{1}{2}\left[\overline{f}(x+ct)+\overline{f}(x-ct)\right],$$

where \overline{f} is the odd 2*L*-periodic extension of *f*.



Remark

Note that the two parts of

$$u(x,t) = \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x+ct) + \frac{1}{2} \sum_{n=1}^{\infty} A_n \sin \frac{n\pi}{L} (x-ct)$$

are Fourier sine series of f evaluated at x + ct and x - ct, respectively.

Therefore

$$u(x,t)=\frac{1}{2}\left[\overline{f}(x+ct)+\overline{f}(x-ct)\right],$$

where \overline{f} is the odd 2*L*-periodic extension of *f*.

Remark

This shows that we can get the solution of the 1D wave equation without actually summing the infinite series!

$$u(x,t)=\frac{1}{2}\left[\overline{f}(x+ct)+\overline{f}(x-ct)\right],$$

is known as <u>d'Alembert's solution</u>, after <u>Jean d'Alembert</u> who first formulated the 1D wave equation and proposed this form of the solution in 1746 – 22 years before Fourier's birth.



$$u(x,t)=\frac{1}{2}\left[\bar{f}(x+ct)+\bar{f}(x-ct)\right],$$

is known as <u>d'Alembert's solution</u>, after <u>Jean d'Alembert</u> who first formulated the 1D wave equation and proposed this form of the solution in 1746 – 22 years before Fourier's birth. It can be interpreted as the <u>average of two traveling waves</u>:

- one traveling to the left,
- the other to the right
- both with speed c.



$$u(x,t)=\frac{1}{2}\left[\overline{f}(x+ct)+\overline{f}(x-ct)\right],$$

is known as <u>d'Alembert's solution</u>, after <u>Jean d'Alembert</u> who first formulated the 1D wave equation and proposed this form of the solution in 1746 – 22 years before Fourier's birth. It can be interpreted as the <u>average of two traveling waves</u>:

- one traveling to the left,
- the other to the right
- both with speed c.

This is illustrated in the Mathematica notebook Wave.nb.



$$u(x,t)=\frac{1}{2}\left[\bar{f}(x+ct)+\bar{f}(x-ct)\right],$$

is known as d'Alembert's solution, after <u>Jean d'Alembert</u> who first formulated the 1D wave equation and proposed this form of the solution in 1746 – 22 years before Fourier's birth. It can be interpreted as the <u>average</u> of two traveling waves:

- one traveling to the left,
- the other to the right
- both with speed c.

This is illustrated in the Mathematica notebook Wave.nb.

Remark

The traveling wave solution is closely related to the solution of PDEs by the method of characteristics (see Chapter 12 in [Haberman] and MATH 489).

Outline

- Derivation of Vertically Vibrating Strings
- 2 Boundary Conditions
- 3 Example: Vibrating String with Fixed Ends
- Membranes (omitted now, done later in Chapter 7)



References I



R. Haberman.

Applied Partial Differential Equations.

Pearson (5th ed.), Upper Saddle River, NJ, 2012.



