

MATH 461: Fourier Series and Boundary Value Problems

Chapter I: The Heat Equation

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Outline

- 1 Mathematical Modeling
- 2 Introduction
- 3 Heat Conduction in a 1D Rod
- 4 Initial and Boundary Conditions
- 5 Equilibrium (or steady-state) Temperature Distribution
- 6 Derivation of the Heat Equation in 2D and 3D



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- 3 Heat Conduction in a 1D Rod
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Physical problem \longrightarrow mathematical model \longrightarrow approximate solution of problem (analytic or numeric)



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- possible roundoff or truncation errors in numerical solutions



Physical Problem

Cars traveling on the Chicago highway system.

How long does it take to get from A to B ? How fast are cars able to travel at any specific position and time?



Math for traffic info services (e.g., [GCM Travel](#))



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Mathematical Model

Cars travel on an idealized one-lane road (no on- or off-ramps, no passing) – lots of simplification.

Consider a bunch of cars on our road. For each instance in time, t , each car will be at a specific position $x_i(t)$ moving with velocity $v_i(t)$, and we have

$$v_i(t) = \frac{dx_i}{dt}(t), \quad i = 1, \dots, N.$$



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See the example in the Mathematica notebook [Traffic.nb](#).



Refined Mathematical Model

In addition to the velocity field, we now also consider

- the **traffic density** $\rho(x, t)$, i.e., the number of cars per unit length at any position x and time t [cars/km],
- the **traffic flow rate** or **flux** $\phi(x, t)$, i.e., the number of cars per unit time passing at position x and time t [cars/h].



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The two are actually related via the velocity field:

$$\phi(x, t) = \rho(x, t)v(x, t) \quad \left[\frac{\text{cars}}{\text{h}} = \frac{\text{cars km}}{\text{km h}} \right]$$



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How might we be able to compute one of these, say the density?



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where

$$N(t) = \int_A^B \rho(x, t) dx. \quad (2)$$



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Therefore, assuming the density ρ is continuous and A, B are const.,

$$\begin{aligned} \int_A^B \frac{\partial}{\partial t} \rho(x, t) dx &= - \int_A^B \frac{\partial}{\partial x} \phi(x, t) dx \\ \iff \int_A^B \left[\frac{\partial}{\partial t} \rho(x, t) + \frac{\partial}{\partial x} \phi(x, t) \right] dx &= 0 \end{aligned}$$



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This gives rise to the **partial differential equation** (see Section 12.6 of [Haberman])

$$\begin{aligned} \frac{\partial}{\partial t} \rho(x, t) &= - \frac{\partial}{\partial x} \phi(x, t) \\ \text{or } \frac{\partial}{\partial t} \rho(x, t) &= - \frac{\partial}{\partial x} [\rho(x, t) v(x, t)] \end{aligned}$$



Even though the traffic flow equation

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is a **first-order** PDE it is more complicated to study than the **second-order** equations we will be looking at in this course since the traffic flow equation may develop a **discontinuous solution** or **shock** – even for a smooth initial condition (see the image in `Traffic.nb`).

The technique required to solve the traffic flow equation is discussed in MATH 489.



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A nice Java applet simulating traffic flow (including shocks) can be found [here](#) and an html5 version [here](#).



Modeling Summary

There are many other kinds of mathematical modeling situations such as

- *data fitting* (e.g., find the best approximation – from a certain linear/nonlinear function class – to given measurement data)
- *parameter estimation* (e.g., find the best parameters for one of the models used earlier – drag coefficient, birth/death rate, etc.)
- *statistical/probabilistic modeling* (e.g., non-deterministic models in finance or weather prediction)
- *discrete modeling* (e.g., determining the best location of a fire department or hospital on a network of roads)
- *geometric modeling* (e.g., used for CAD systems)
- *asymptotic modeling* (focus on extreme or limiting cases, can usually be done analytically)



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An entertaining overview of the field of mathematical modeling is provided by Charlie's activities on the TV show *NUMB3RS*.



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We will formulate a model which describes **how the temperature u changes** over **time t** in a **region** (1D $\rightarrow x$, 2D $\rightarrow (x, y)$, or 3D $\rightarrow (x, y, z)$).



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Since **u is always at least a function of two variables**, e.g., $u = u(x, t)$, this will lead to a **partial differential equation** or **PDE** involving the unknown function u along with its (partial) derivatives with respect to space and time, i.e., u_t, u_x, u_y, u_{xx} , etc.



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Our models will also require certain **initial** and **boundary conditions** such as the entire temperature distribution at the beginning and the temperature on the boundary at any time t .



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We will focus on **heat conduction**.



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Our derivation will consist of two steps:

- 1 We use an **energy conservation principle** to derive a PDE for the heat energy in a one-dimensional rod.

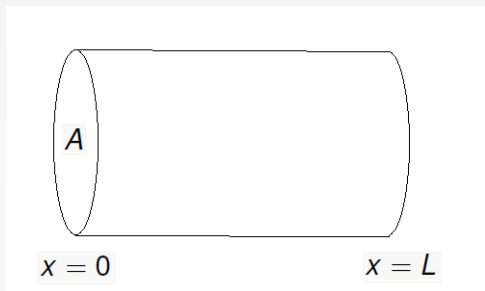


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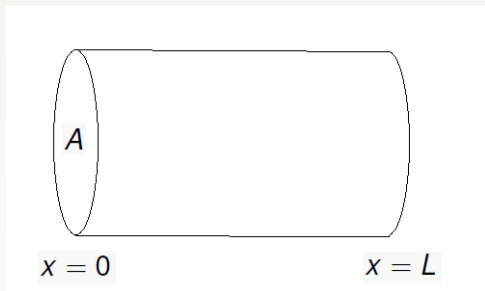
- 1 We use an **energy conservation principle** to derive a PDE for the heat energy in a one-dimensional rod.
- 2 Then we use **Fourier's law of heat conduction** to relate heat energy to temperature to obtain the so-called **heat equation**, a PDE that models the temperature in the rod at any position x and time t .



We consider a rod of length L and cross section A



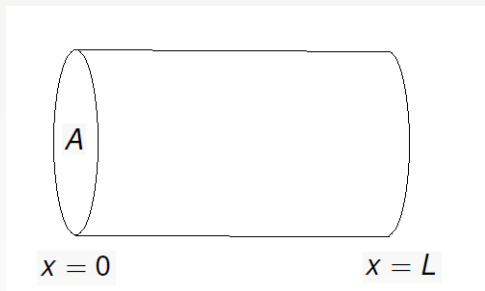
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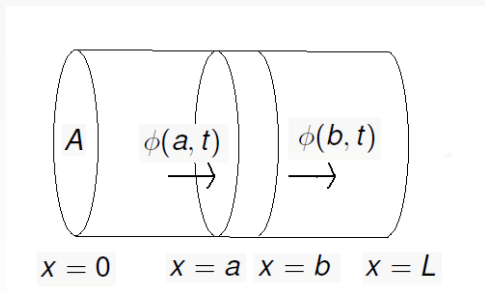
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Remark

*We assume that e depends only on x and t . This means that the rod is **insulated** (except possibly at the ends) so that heat can only flow in the x -direction.*

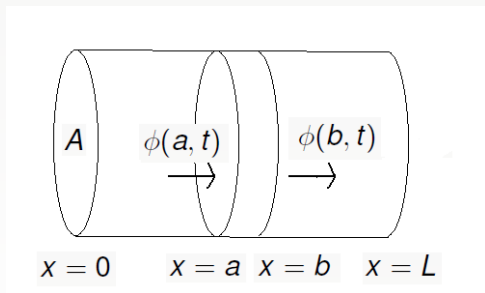
Similar to the traffic flow problem we also consider:

- The **heat flux** or **heat flow rate** $\phi(x, t)$, i.e., the amount of heat energy per unit time flowing (from left to right) through a unit cross-sectional area at x . Thus, $\phi(x, t) > 0$ denotes flow to right and $\phi(x, t) < 0$ flow to left.



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- Possible **heat sources** $Q(x, t)$, i.e., the amount of heat energy per unit volume generated per unit time.



Conservation of Energy

This is the major physical assumption used:

$$\begin{aligned} & \{\text{Rate of change of heat energy between } x = a \text{ and } x = b\} \\ & \quad = \\ & \quad \quad \{\text{rate of heat energy flowing through ends}\} \\ & \quad \quad + \\ & \quad \quad \{\text{rate of heat energy generated inside segment of rod}\} \end{aligned}$$

Remark

*Note that all of these are rates of change **per unit of time**.*



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Rate of heat energy generated inside: $A \int_a^b Q(x, t) dx$.

Together (conservation of energy – integral form):

$$\frac{d}{dt} \int_a^b e(x, t) dx = \phi(a, t) - \phi(b, t) + \int_a^b Q(x, t) dx \quad (3)$$

We can further manipulate (3):

First, provided that e is continuous and a, b are const. wrt t ,

$$\frac{d}{dt} \int_a^b e(x, t) dx = \int_a^b \frac{\partial}{\partial t} e(x, t) dx.$$



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or

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Since

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Remark

Equation (3) is more general than (4) since it also applies if e and ϕ are not continuous.

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Units:

$$\left[\frac{J}{m} \right] = \left[\frac{J}{kg^\circ C} \right] \left[\frac{kg}{m} \right] [^\circ C]$$



We can now modify the conservation of energy equation (4)

$$\frac{\partial}{\partial t} e(x, t) = -\frac{\partial}{\partial x} \phi(x, t) + Q(x, t)$$

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Remark

This is still not ideal since it involves both temperature and energy flux. We need to unify further.



Fourier's Law of Heat Conduction

The final physical principle that makes everything come together.



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- The greater these differences, the greater the flux, i.e., $\phi \propto \frac{\partial}{\partial x} u$.
- Heat flow depends on the specific material of the rod.

The resulting formula is

$$\phi(x, t) = -K_0(x) \frac{\partial}{\partial x} u(x, t),$$

where the **thermal conductivity** K_0 depends on the material.

Remark

The “-” is needed since $\phi > 0$ indicates flow from left to right, but energy also flows from hot to cold and $\frac{\partial}{\partial x} u(x, t) < 0$ if it is warmer on the left.

Using Fourier's law of heat conduction

$$\phi(x, t) = -K_0(x) \frac{\partial}{\partial x} u(x, t),$$

we can rewrite (5) as

$$c(x)\rho(x) \frac{\partial}{\partial t} u(x, t) = \frac{\partial}{\partial x} \left[K_0(x) \frac{\partial}{\partial x} u(x, t) \right] + Q(x, t).$$

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In most cases we will **assume c, ρ, K_0 to be constant**, i.e., we will use a uniform material. Then we get

$$c\rho \frac{\partial}{\partial t} u(x, t) = K_0 \frac{\partial^2}{\partial x^2} u(x, t) + Q(x, t)$$



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$$c\rho \frac{\partial}{\partial t} u(x, t) = K_0 \frac{\partial^2}{\partial x^2} u(x, t) + Q(x, t)$$

or

$$\frac{\partial}{\partial t} u(x, t) = k \frac{\partial^2}{\partial x^2} u(x, t) + q(x, t),$$

where $k = \frac{K_0}{c\rho}$, the **thermal diffusivity** and $q(x, t) = \frac{Q(x, t)}{c\rho}$.



Finally, if no sources are present, i.e., $Q(x, t) = 0$, then

$$\frac{\partial}{\partial t} u(x, t) = k \frac{\partial^2}{\partial x^2} u(x, t) \quad (6)$$

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Remark

The same form of equation also applies to many other situations, such as diffusion of pollutants, etc.



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- 2 Introduction
- 3 Heat Conduction in a 1D Rod
- 4 Initial and Boundary Conditions**
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Initial Condition

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The two conditions demanded by $\frac{\partial^2 u}{\partial x^2}$ are discussed next.

Remark

*As we will see later, one cannot just add **any** set of conditions. They should be chosen such that the problem is **well-posed**, i.e., it should allow for the **existence** of a **unique solution** that depends **continuously** on the given conditions.*

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Controlled end temperature: e.g., using baths at the ends

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Newton's law of cooling: e.g., cooler air is passed by ends of rod



For Newton's law of cooling we assume there is only partial insulation governed by a positive **heat transfer** (or convection) **coefficient** H , e.g.,

$$\phi(0, t) = -H [u(0, t) - u_{B_1}(t)] \quad (\text{Newton's law})$$

Note “ $-$ ” which indicates that – for a rod that is hotter than its environment – heat flow is negative, i.e., flows to the cooler environment (on the “left”).



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We also note that

- $H \rightarrow 0$ corresponds to perfect insulation
- $H \rightarrow \infty$ corresponds to controlled temperature



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We are now ready to solve our first heat equation PDEs. We

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- consider **different types of boundary conditions**
 - fixed end temperature
 - insulated ends
- under the **fundamental simplifying assumption** that we have observed the temperature distribution process for a long time and it has settled down to an **equilibrium temperature distribution**, i.e., the **temperature no longer changes with time**.



Controlled End Temperature

Problem:

$$\frac{\partial u}{\partial t}(x, t) = k \frac{\partial^2 u}{\partial x^2}(x, t)$$

$$u(x, 0) = f(x) \quad (\text{initial condition})$$

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The IC becomes meaningless¹, and the BCs become

$$u(0) = T_1, \quad u(L) = T_2.$$

¹but should be consistent with the BCs



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Therefore

$$u(x) = T_1 + \frac{T_2 - T_1}{L}x,$$

i.e., the temperature distribution interpolates linearly between the fixed end temperatures.



Remark

We will later see that the time *dependent* PDE problem

$$\begin{aligned}\frac{\partial u}{\partial t}(x, t) &= k \frac{\partial^2 u}{\partial x^2}(x, t) \\ u(x, 0) &= f(x)\end{aligned}$$

with time *independent* BCs

$$u(0, t) = T_1, \quad u(L, t) = T_2$$

has (in the limit – for very large time) the steady-state solution we just computed, so in this case one can just solve the simple equilibrium problem from the previous slide.



Insulated Boundaries

Now we have

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Its general solution (again via integration) is

$$u(x) = C_1 x + C_2.$$



If we try to use our BCs to determine C_1, C_2 we note that **either one of the BCs** implies

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Remark

- Note that the ODE problem (7) is **not well posed**. It does not have a unique solution.
- One might expect that the **initial temperature distribution $f(x)$** should affect C_2 .
- In general one should not expect $u(x) = f(x)$, but rather that the initial distribution somehow “levels out”.

Since thermal energy is conserved inside the rod, we can go back to the **integral form** of the conservation of energy law (3):

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$$\int_0^L c\rho u(x, t) dx = \text{const} \quad (\text{total heat energy})$$



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In summary, we get

$$u(x) = \frac{1}{L} \int_0^L f(x)dx,$$

i.e., the steady-state temperature distribution is the **average** of the initial temperature distribution.



Outline

- 1 Mathematical Modeling
- 2 Introduction
- 3 Heat Conduction in a 1D Rod
- 4 Initial and Boundary Conditions
- 5 Equilibrium (or steady-state) Temperature Distribution
- 6 Derivation of the Heat Equation in 2D and 3D**



Derivation of the Heat Equation in 2D and 3D

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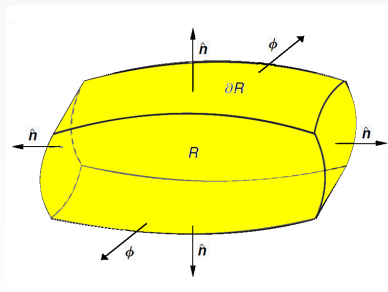
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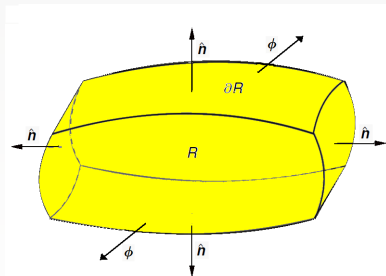
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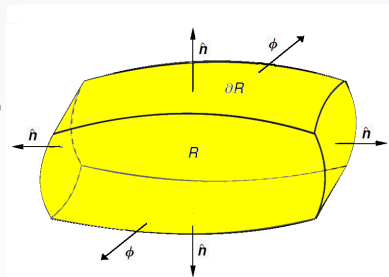
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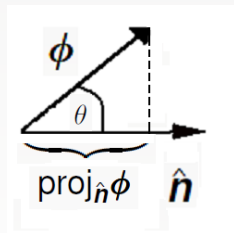


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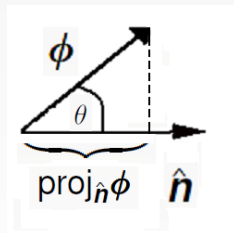
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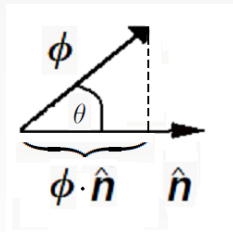
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Theorem (Divergence/Gauss/Ostrogradsky)

Suppose R is a bounded region in \mathbb{R}^3 with piecewise smooth boundary ∂R . If $\mathbf{f} = (f_1, f_2, f_3) \in C^1$ in an open region that contains R then

$$\iiint_R \nabla \cdot \mathbf{f}(x, y, z) \, dV = \iint_{\partial R} \mathbf{f}(x, y, z) \cdot \hat{\mathbf{n}}(x, y, z) \, dS,$$

where $\nabla \cdot \mathbf{f} = \frac{\partial}{\partial x} f_1 + \frac{\partial}{\partial y} f_2 + \frac{\partial}{\partial z} f_3 = \operatorname{div} \mathbf{f}$ and $\hat{\mathbf{n}}(x, y, z)$ is the unit outward normal vector to R at the point (x, y, z) of ∂R .



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- This is the 3D-analogue of the FT of Calculus.
- In 2D we would be using *Green's theorem*.

Conservation of Energy (again)

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We need to derive formulas for each one of these three parts.



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Similarly, the **rate of heat energy generated inside of R** is

$$\iiint_R Q(x, y, z, t) dV \quad (10)$$



Using only the normal component of the heat flux (see (8)) we get the rate of heat energy flowing through boundary surface:

$$- \iint_{\partial R} \phi(x, y, z, t) \cdot \hat{\mathbf{n}}(x, y, z) \, dS \quad (11)$$



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The “-” sign appears since outward flow ϕ is positive, but such a flow reduces the heat energy.



Combining (9–11) the conservation of energy principle gives:

$$\frac{d}{dt} \iiint_R c\rho u dV = - \iint_{\partial R} \phi \cdot \hat{\mathbf{n}} dS + \iiint_R Q dV \quad (12)$$



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This is where we will use the **divergence theorem**, i.e.,

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Since this holds for **arbitrary** R we get (compare with (5))

$$c(x, y, z)\rho(x, y, z) \frac{\partial}{\partial t} u(x, y, z, t) = -\nabla \cdot \phi(x, y, z, t) + Q(x, y, z, t)$$



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$$\phi \cdot \hat{\mathbf{n}} = 0 \quad \iff \quad \nabla u \cdot \hat{\mathbf{n}} = 0,$$

i.e., the **normal derivative of u** is zero.



- Boundary conditions (cont.)
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- Note that $\hat{\mathbf{n}} = \mathbf{i}$ and $\hat{\mathbf{n}} = -\mathbf{i}$ correspond to 1D end conditions.
For example,

$$\nabla u \cdot \mathbf{i} = \left(\frac{\partial u}{\partial x}, \frac{\partial u}{\partial y}, \frac{\partial u}{\partial z} \right) \cdot (1, 0, 0) = \frac{\partial u}{\partial x}$$



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If in addition $Q = 0$, then we get

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- Now the *steady state equations are PDEs*, and we need to *postpone their solution until later*.
- In 2D these equations look the same, except that we use the *2D Laplacian*

$$\nabla^2 u = \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}.$$



Other Coordinate Systems

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⇒ need to convert the Laplacian to cylindrical and spherical coordinates

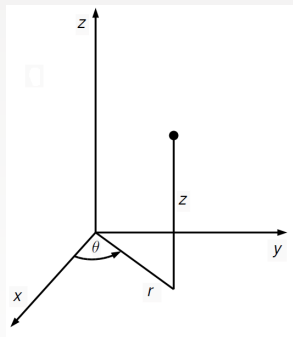


Cylindrical Coordinates

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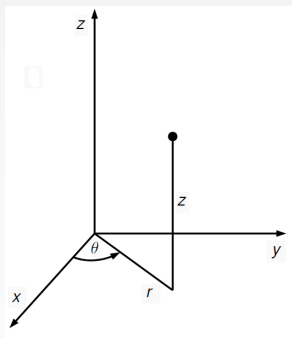


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These coordinates imply $r = \sqrt{x^2 + y^2}$ and $\theta = \tan^{-1} \frac{y}{x}$ and so

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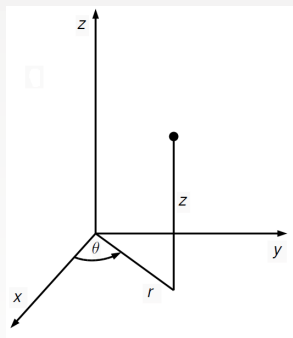


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Therefore the derivatives $\frac{\partial^2 u}{\partial x^2}$, $\frac{\partial^2 u}{\partial y^2}$, $\frac{\partial^2 u}{\partial z^2}$ can be expressed using the chain rule.



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$$\begin{aligned}
 \frac{\partial u}{\partial x} &= \frac{\partial u}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial u}{\partial \theta} \frac{\partial \theta}{\partial x} \\
 &= \frac{\partial u}{\partial r} \frac{2x}{2 \underbrace{\sqrt{x^2 + y^2}}_{=r}} + \frac{\partial u}{\partial \theta} \underbrace{\frac{-\frac{y}{x^2}}{1 + \left(\frac{y}{x}\right)^2}}_{=\frac{-y}{x^2+y^2} = \frac{-y}{r^2}} \\
 &= \frac{\partial u}{\partial r} \frac{x}{r} - \frac{\partial u}{\partial \theta} \frac{y}{r^2}
 \end{aligned}$$



First calculate

$$\begin{aligned}
 \frac{\partial u}{\partial x} &= \frac{\partial u}{\partial r} \frac{\partial r}{\partial x} + \frac{\partial u}{\partial \theta} \frac{\partial \theta}{\partial x} \\
 &= \frac{\partial u}{\partial r} \frac{2x}{2 \underbrace{\sqrt{x^2 + y^2}}_{=r}} + \frac{\partial u}{\partial \theta} \underbrace{\frac{-\frac{y}{x^2}}{1 + \left(\frac{y}{x}\right)^2}}_{=\frac{-y}{x^2+y^2} = \frac{-y}{r^2}} \\
 &= \frac{\partial u}{\partial r} \frac{x}{r} - \frac{\partial u}{\partial \theta} \frac{y}{r^2}
 \end{aligned}$$

Using $x = r \cos \theta$ and $y = r \sin \theta$ we get

$$\frac{\partial u}{\partial x} = \cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta}$$

and so the differential operator

$$\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}$$



Next, using $\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}$ three times we get

$$\frac{\partial^2 u}{\partial x^2} = \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} \right) = \cos \theta \frac{\partial}{\partial r} \left(\frac{\partial u}{\partial x} \right) - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left(\frac{\partial u}{\partial x} \right)$$



Next, using $\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}$ three times we get

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} \right) = \cos \theta \frac{\partial}{\partial r} \left(\frac{\partial u}{\partial x} \right) - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left(\frac{\partial u}{\partial x} \right) \\ &= \cos \theta \frac{\partial}{\partial r} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] \end{aligned}$$



Next, using $\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}$ three times we get

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} \right) = \cos \theta \frac{\partial}{\partial r} \left(\frac{\partial u}{\partial x} \right) - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left(\frac{\partial u}{\partial x} \right) \\ &= \cos \theta \frac{\partial}{\partial r} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] \end{aligned}$$

Differentiation using the product rule along with $\frac{\partial^2}{\partial r \partial \theta} = \frac{\partial^2}{\partial \theta \partial r}$ gives us

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \cos \theta \left[\cos \theta \frac{\partial^2 u}{\partial r^2} + \frac{\sin \theta}{r^2} \frac{\partial u}{\partial \theta} - \frac{\sin \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} \right] \\ &\quad - \frac{\sin \theta}{r} \left[-\sin \theta \frac{\partial u}{\partial r} + \cos \theta \frac{\partial^2 u}{\partial r \partial \theta} - \frac{\cos \theta}{r} \frac{\partial u}{\partial \theta} - \frac{\sin \theta}{r} \frac{\partial^2 u}{\partial \theta^2} \right] \end{aligned}$$



Next, using $\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}$ three times we get

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} \right) = \cos \theta \frac{\partial}{\partial r} \left(\frac{\partial u}{\partial x} \right) - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left(\frac{\partial u}{\partial x} \right) \\ &= \cos \theta \frac{\partial}{\partial r} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left[\cos \theta \frac{\partial u}{\partial r} - \frac{\sin \theta}{r} \frac{\partial u}{\partial \theta} \right] \end{aligned}$$

Differentiation using the product rule along with $\frac{\partial^2}{\partial r \partial \theta} = \frac{\partial^2}{\partial \theta \partial r}$ gives us

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \cos \theta \left[\cos \theta \frac{\partial^2 u}{\partial r^2} + \frac{\sin \theta}{r^2} \frac{\partial u}{\partial \theta} - \frac{\sin \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} \right] \\ &\quad - \frac{\sin \theta}{r} \left[-\sin \theta \frac{\partial u}{\partial r} + \cos \theta \frac{\partial^2 u}{\partial r \partial \theta} - \frac{\cos \theta}{r} \frac{\partial u}{\partial \theta} - \frac{\sin \theta}{r} \frac{\partial^2 u}{\partial \theta^2} \right] \end{aligned}$$

Therefore

$$\begin{aligned} \frac{\partial^2 u}{\partial x^2} &= \cos^2 \theta \frac{\partial^2 u}{\partial r^2} + 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} - 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} \\ &\quad + \frac{\sin^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\sin^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2} \end{aligned}$$



We just calculated

$$\frac{\partial^2 u}{\partial x^2} = \cos^2 \theta \frac{\partial^2 u}{\partial r^2} + 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} - 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\sin^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\sin^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Analogously

$$\frac{\partial^2 u}{\partial y^2} = \sin^2 \theta \frac{\partial^2 u}{\partial r^2} - 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} + 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\cos^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\cos^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$



We just calculated

$$\frac{\partial^2 u}{\partial x^2} = \cos^2 \theta \frac{\partial^2 u}{\partial r^2} + 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} - 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\sin^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\sin^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Analogously

$$\frac{\partial^2 u}{\partial y^2} = \sin^2 \theta \frac{\partial^2 u}{\partial r^2} - 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} + 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\cos^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\cos^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Therefore

$$\nabla^2 u = \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2}$$



We just calculated

$$\frac{\partial^2 u}{\partial x^2} = \cos^2 \theta \frac{\partial^2 u}{\partial r^2} + 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} - 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\sin^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\sin^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Analogously

$$\frac{\partial^2 u}{\partial y^2} = \sin^2 \theta \frac{\partial^2 u}{\partial r^2} - 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} + 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\cos^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\cos^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Therefore

$$\begin{aligned} \nabla^2 u &= \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \\ &= (\cos^2 \theta + \sin^2 \theta) \frac{\partial^2 u}{\partial r^2} + \left(\frac{\sin^2 \theta}{r} + \frac{\cos^2 \theta}{r} \right) \frac{\partial u}{\partial r} + \left(\frac{\sin^2 \theta}{r^2} + \frac{\cos^2 \theta}{r^2} \right) \frac{\partial^2 u}{\partial \theta^2} + \frac{\partial^2 u}{\partial z^2} \end{aligned}$$



We just calculated

$$\frac{\partial^2 u}{\partial x^2} = \cos^2 \theta \frac{\partial^2 u}{\partial r^2} + 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} - 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\sin^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\sin^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Analogously

$$\frac{\partial^2 u}{\partial y^2} = \sin^2 \theta \frac{\partial^2 u}{\partial r^2} - 2 \frac{\sin \theta \cos \theta}{r^2} \frac{\partial u}{\partial \theta} + 2 \frac{\sin \theta \cos \theta}{r} \frac{\partial^2 u}{\partial r \partial \theta} + \frac{\cos^2 \theta}{r} \frac{\partial u}{\partial r} + \frac{\cos^2 \theta}{r^2} \frac{\partial^2 u}{\partial \theta^2}$$

Therefore

$$\begin{aligned} \nabla^2 u &= \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \\ &= (\cos^2 \theta + \sin^2 \theta) \frac{\partial^2 u}{\partial r^2} + \left(\frac{\sin^2 \theta}{r} + \frac{\cos^2 \theta}{r} \right) \frac{\partial u}{\partial r} + \left(\frac{\sin^2 \theta}{r^2} + \frac{\cos^2 \theta}{r^2} \right) \frac{\partial^2 u}{\partial \theta^2} + \frac{\partial^2 u}{\partial z^2} \end{aligned}$$

or

Laplacian in cylindrical coordinates:

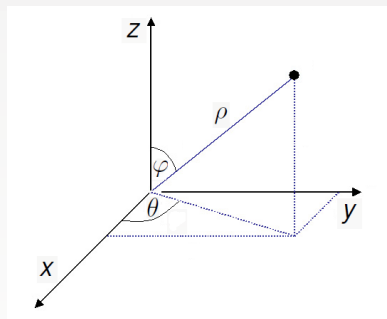
$$\nabla^2 u = \frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} + \frac{1}{r^2} \frac{\partial^2 u}{\partial \theta^2} + \frac{\partial^2 u}{\partial z^2}$$

Spherical Coordinates

$$x = \rho \sin \varphi \cos \theta$$

$$y = \rho \sin \varphi \sin \theta$$

$$z = \rho \cos \varphi$$

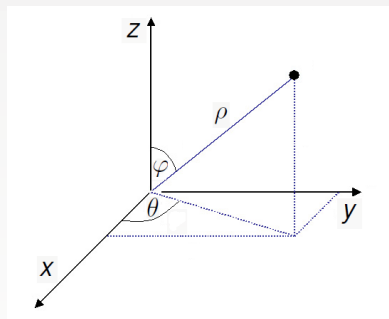


Spherical Coordinates

$$x = \rho \sin \varphi \cos \theta$$

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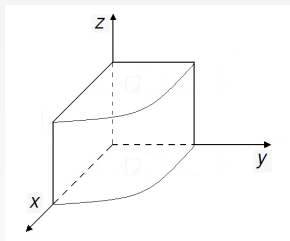
Proceeding similarly as for cylindrical coordinates one can obtain

Laplacian in spherical coordinates:

$$\nabla^2 u = \frac{1}{\rho^2} \frac{\partial}{\partial \rho} \left[\rho^2 \frac{\partial u}{\partial \rho} \right] + \frac{1}{\rho^2 \sin \varphi} \frac{\partial}{\partial \varphi} \left[\sin \varphi \frac{\partial u}{\partial \varphi} \right] + \frac{1}{\rho^2 \sin^2 \varphi} \frac{\partial^2 u}{\partial \theta^2}$$

Example

Let $u(r, \theta)$ denote the temperature, independent of z , in a long rod parallel to the z -axis whose cross-section in the xy -plane is given by the circular sector $0 \leq r \leq 1$, $0 \leq \theta \leq \frac{\pi}{2}$.

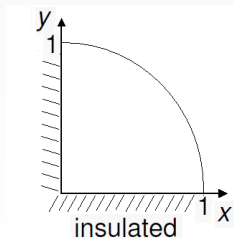


(a) Show

$$\frac{\partial u}{\partial \theta} = -y \frac{\partial u}{\partial x} + x \frac{\partial u}{\partial y}$$

(b) Use the result of (a) to show that if the rod is insulated on its planar surfaces, where $\theta = 0$ and $\theta = \frac{\pi}{2}$, then u must satisfy the boundary conditions

$$\frac{\partial u}{\partial \theta}(r, 0) = 0, \quad \frac{\partial u}{\partial \theta}(r, \frac{\pi}{2}) = 0, \quad 0 < r < 1.$$



Solution

(a) We use polar coordinates

$$x = r \cos \theta, \quad y = r \sin \theta$$



Solution

(a) We use polar coordinates

$$x = r \cos \theta, \quad y = r \sin \theta$$

Then $u(x, y) = u(x(r, \theta), y(r, \theta))$ and the chain rule gives

$$\frac{\partial u}{\partial \theta} = \frac{\partial u}{\partial x} \frac{\partial x}{\partial \theta} + \frac{\partial u}{\partial y} \frac{\partial y}{\partial \theta}$$



Solution

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Then $u(x, y) = u(x(r, \theta), y(r, \theta))$ and the chain rule gives

$$\begin{aligned} \frac{\partial u}{\partial \theta} &= \frac{\partial u}{\partial x} \frac{\partial x}{\partial \theta} + \frac{\partial u}{\partial y} \frac{\partial y}{\partial \theta} \\ &= \frac{\partial u}{\partial x} (-r \sin \theta) + \frac{\partial u}{\partial y} (r \cos \theta) \end{aligned}$$



Solution

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- (b) Let $\hat{\mathbf{n}}$ be the **unit outer normal vector** and remember that insulated means that

$$\phi \cdot \hat{\mathbf{n}} = 0 \quad \xLeftrightarrow{\text{Fourier's law}} \quad -K_0 \nabla u \cdot \hat{\mathbf{n}} = 0$$

so that $\nabla u \cdot \hat{\mathbf{n}} = 0$, where $\nabla u = (u_x, u_y)$.



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Face $\theta = 0$: Here $\hat{\mathbf{n}} = (0, -1)$ (in cartesian coordinates). Therefore

$$\nabla u \cdot \hat{\mathbf{n}} = (u_x, u_y) \cdot (0, -1) = -\frac{\partial u}{\partial y}$$



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Now

$$\frac{\partial u}{\partial \theta}(r, 0) \stackrel{(a)}{=} -y(r, 0) \frac{\partial u}{\partial x}(r, 0) + x(r, 0) \frac{\partial u}{\partial y}(r, 0)$$



(b) Let $\hat{\mathbf{n}}$ be the **unit outer normal vector** and remember that insulated means that

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Now

$$\begin{aligned} \frac{\partial u}{\partial \theta}(r, 0) &\stackrel{(a)}{=} -y(r, 0) \frac{\partial u}{\partial x}(r, 0) + x(r, 0) \frac{\partial u}{\partial y}(r, 0) \\ &= -r \sin \theta|_{\theta=0} \frac{\partial u}{\partial x}(r, 0) + r \cos \theta|_{\theta=0} \frac{\partial u}{\partial y}(r, 0) \end{aligned}$$



- (b) Let $\hat{\mathbf{n}}$ be the **unit outer normal vector** and remember that insulated means that

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$$\phi \cdot \hat{\mathbf{n}} = 0 \quad \text{Fourier's law} \quad \Longleftrightarrow \quad -K_0 \nabla u \cdot \hat{\mathbf{n}} = 0$$

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Now

$$\begin{aligned} \frac{\partial u}{\partial \theta}(r, 0) &\stackrel{(a)}{=} -y(r, 0) \frac{\partial u}{\partial x}(r, 0) + x(r, 0) \frac{\partial u}{\partial y}(r, 0) \\ &= \underbrace{-r \sin \theta|_{\theta=0}}_{=0} \frac{\partial u}{\partial x}(r, 0) + r \cos \theta|_{\theta=0} \underbrace{\frac{\partial u}{\partial y}(r, 0)}_{=0 \text{ } (\nabla u \cdot \hat{\mathbf{n}}=0)} \end{aligned}$$

Therefore

$$\frac{\partial u}{\partial \theta}(r, 0) = 0.$$



(b) (cont.)

Face $\theta = \frac{\pi}{2}$: Here $\hat{\mathbf{n}} = (-1, 0)$ so that $\nabla u \cdot \hat{\mathbf{n}} = -\frac{\partial u}{\partial x}$.



(b) (cont.)

Face $\theta = \frac{\pi}{2}$: Here $\hat{\mathbf{n}} = (-1, 0)$ so that $\nabla u \cdot \hat{\mathbf{n}} = -\frac{\partial u}{\partial x}$.

Now

$$\frac{\partial u}{\partial \theta}\left(r, \frac{\pi}{2}\right) \stackrel{(a)}{=} -y\left(r, \frac{\pi}{2}\right) \frac{\partial u}{\partial x}\left(r, \frac{\pi}{2}\right) + x\left(r, \frac{\pi}{2}\right) \frac{\partial u}{\partial y}\left(r, \frac{\pi}{2}\right)$$



(b) (cont.)

Face $\theta = \frac{\pi}{2}$: Here $\hat{\mathbf{n}} = (-1, 0)$ so that $\nabla u \cdot \hat{\mathbf{n}} = -\frac{\partial u}{\partial x}$.

Now

$$\begin{aligned} \frac{\partial u}{\partial \theta}\left(r, \frac{\pi}{2}\right) &\stackrel{(a)}{=} -y\left(r, \frac{\pi}{2}\right) \frac{\partial u}{\partial x}\left(r, \frac{\pi}{2}\right) + x\left(r, \frac{\pi}{2}\right) \frac{\partial u}{\partial y}\left(r, \frac{\pi}{2}\right) \\ &= -r \sin \frac{\pi}{2} \frac{\partial u}{\partial x}\left(r, \frac{\pi}{2}\right) + r \cos \frac{\pi}{2} \frac{\partial u}{\partial y}\left(r, \frac{\pi}{2}\right) \end{aligned}$$



(b) (cont.)

Face $\theta = \frac{\pi}{2}$: Here $\hat{\mathbf{n}} = (-1, 0)$ so that $\nabla u \cdot \hat{\mathbf{n}} = -\frac{\partial u}{\partial x}$.

Now

$$\begin{aligned} \frac{\partial u}{\partial \theta} \left(r, \frac{\pi}{2} \right) &\stackrel{(a)}{=} -y \left(r, \frac{\pi}{2} \right) \frac{\partial u}{\partial x} \left(r, \frac{\pi}{2} \right) + x \left(r, \frac{\pi}{2} \right) \frac{\partial u}{\partial y} \left(r, \frac{\pi}{2} \right) \\ &= -r \sin \frac{\pi}{2} \underbrace{\frac{\partial u}{\partial x} \left(r, \frac{\pi}{2} \right)}_{=0 \text{ } (\nabla u \cdot \hat{\mathbf{n}}=0)} + r \cos \frac{\pi}{2} \underbrace{\frac{\partial u}{\partial y} \left(r, \frac{\pi}{2} \right)}_{=0} \end{aligned}$$



(b) (cont.)

Face $\theta = \frac{\pi}{2}$: Here $\hat{\mathbf{n}} = (-1, 0)$ so that $\nabla u \cdot \hat{\mathbf{n}} = -\frac{\partial u}{\partial x}$.

Now



$$\begin{aligned} \frac{\partial u}{\partial \theta}(r, \frac{\pi}{2}) &\stackrel{(a)}{=} -y(r, \frac{\pi}{2}) \frac{\partial u}{\partial x}(r, \frac{\pi}{2}) + x(r, \frac{\pi}{2}) \frac{\partial u}{\partial y}(r, \frac{\pi}{2}) \\ &= -r \sin \frac{\pi}{2} \underbrace{\frac{\partial u}{\partial x}(r, \frac{\pi}{2})}_{=0 (\nabla u \cdot \hat{\mathbf{n}}=0)} + r \cos \frac{\pi}{2} \underbrace{\frac{\partial u}{\partial y}(r, \frac{\pi}{2})}_{=0} \end{aligned}$$

Therefore

$$\frac{\partial u}{\partial \theta}(r, \frac{\pi}{2}) = 0.$$



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